Draft Noise Study Report

US 41/SR 45 AT CSX GRADE SEPARATION FROM S OF SR 676 TO N OF SR 676 Project Development & Environment (PD&E) Study



Florida Department of Transportation

District 7

Work Program Item Segment No. 440749-1

ETDM Project No. 14345

Hillsborough County, Florida

February 2023

The environmental review, consultation, and other actions required by applicable federal environmental laws for this project are being, or have been, carried out by FDOT pursuant to 23 U.S.C. §327 and a Memorandum of Understanding dated May 26, 2022 and executed by the Federal Highway Administration and FDOT.

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FROM S OF SR 676 TO N OF SR 676

Project Development & Environment (PD&E) Study

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Prepared for:



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Executive Summary

The Florida Department of Transportation (FDOT) is conducting a Design Change and Right of Way (ROW) Authorization Reevaluation of a previous Environmental Assessment (EA) (Work Program Item Segment (WPIS) No. 255598-1) with a Finding of No Significant Impact (FONSI) approved by the Federal Highway Administration on May 24, 1994. The current study effort being conducted under WPIS No. 440749-1 evaluates capacity and operational improvements on US 41/SR 45/SR 599 from south of the Causeway Boulevard intersection to north of the Causeway Boulevard intersection. These improvements include the construction of a grade separation of US 41/SR 45 at the CSX railroad crossing located approximately 1,400 feet south of the Causeway Boulevard intersection. Intersection and operational improvements at US 41/SR 45 and Causeway Boulevard are also provided.

The purpose of this project is to reduce traffic delays associated with the CSX railroad crossing, adequately support the safe movement of vehicle traffic, including trucks and freight, and enhance connectivity and safety for bicyclists and pedestrians.

This Noise Study Report (NSR) presents the assumptions, data, procedures, and results of the traffic noise analysis that was conducted to evaluate the proposed improvements. The objectives of the NSR are to identify noise sensitive receptors (discrete or representative locations of a noise sensitive area) adjacent to the project corridor, to predict and evaluate future traffic noise levels at the receptors with and without the improvements, and to evaluate the need for, and effectiveness of, noise abatement measures. This NSR also discusses construction-related noise and vibration and identifies traffic noise impact areas for future compatible land use planning adjacent to the project corridor.

A total of 55 properties for which there are land use Noise Abatement Criteria (NAC) were evaluated. The properties are comprised of 52 residential properties, one active sports area, one restaurant, and one motel.

The conclusions of this traffic noise analysis are as follows:

- Predicted noise levels will create eleven (11) NAC residential land use impacts to noisesensitive receptors in Common Noise Environments (CNEs) 09, 10, 11 and 12.
- The proposed project will not create any additional noise impacts due substantial noise increase over predicted existing noise levels.
- No noise barriers were found to meet the criteria for feasibility and reasonableness.

The Florida Department of Transportation is committed to the construction of feasible and reasonable noise abatement measures where recommended. However, based on the noise analyses performed to date, there are no feasible and reasonable solutions available to mitigate the noise impacts at CNEs 09, 10, 11, and 12. This determination is subject to a detailed review in Design and subsequent re-evaluations.

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1 INTRODUCTION

1.1 Project Background

The Florida Department of Transportation (FDOT) is conducting a Design Change and Right of Way (ROW) Authorization Reevaluation of a previous Environmental Assessment (EA) (Work Program Item Segment (WPIS) No. 255598-1) with a Finding of No Significant Impact (FONSI) approved by the Federal Highway Administration on May 24, 1994. **Figure 1-1** shows the limits of the previous PD&E study completed along 22nd Street Causeway/Causeway Boulevard (State Road 676) from State Road (SR) 60 to US 301, in Hillsborough County, Florida. The segment currently being evaluated/advanced is shown as Segment 3 on **Figure 1-1**.

The previous study evaluated anticipated conditions for a 2015 Design Year. The FONSI documented the construction of a six-lane roadway to replace the existing 2- to 4-lane roadway beginning at SR 60 and extending approximately 7 miles east at US 301. Since the completion of the 1994 PD&E Study, Causeway Boulevard has been widened to four-lanes.

The project included a new interchange at US 41/Causeway Boulevard intersection for which the approved concept was a "compressed diamond" interchange with US 41 elevated over Causeway Boulevard. This interchange is also known as a Single Point Urban Interchange (SPUI) or a Tight Urban Diamond Interchange (TUDI). The study identified that the US 41 interchange bridge would carry three lanes of traffic in each direction with a barrier wall separating opposing traffic. The study recommended an additional grade separation of US 41 over the CSX railroad crossing south of Causeway Boulevard while the CSX railroad crossing east of US 41 would remain at-grade with Causeway Boulevard. The concept showed the SPUI ramps oriented along US 41 and one-way, one-lane frontage roads were provided in the southeast and northeast quadrants to provide local property access. Five-foot sidewalks and 4-foot bicycle lanes were proposed along both sides of Causeway Boulevard.

The current study effort being conducted under WPIS# 440749-1 is evaluating various intersection and operational improvements along Causeway Boulevard east and west of US 41 (SR 45/SR 599) along US 41 from south of the Causeway Boulevard intersection to north of the Causeway Boulevard intersection. These improvements include the construction of a grade separation of US 41/SR 45 at the CSX railroad crossing located approximately 1,400 feet south of the Causeway Boulevard intersection. Bicycle and pedestrian facility improvements along US 41 and Causeway Boulevard are also provided.



Figure 1-1 Project Location Map

1.2 Project Purpose and Need

<u>Purpose</u>

The purpose of this project is to reduce traffic delays associated with the CSX railroad crossing, adequately support the safe movement of vehicle traffic, including trucks and freight, and enhance connectivity and safety for bicyclists and pedestrians.

Need

As expressed in the original 1994 EA/FONSI, the need for the 22nd Street Causeway/Causeway Boulevard improvements was based on the following criteria: System Linkage; Capacity; Transportation Demand; Federal, State, or Local Government Authority; Socioeconomic Demand; Modal Interrelationships; Safety; and Navigation.

For the current segment, US 41 and Causeway Boulevard are vital arterial highways which serve the City of Tampa located in Hillsborough County. The US 41/SR 45 and Causeway Boulevard intersection experiences traffic delays during the AM and PM peak periods with heavy truck traffic (approximately 13% of the daily volume) traversing through the intersection. The presence of CSX railroad crossings to the south and east of the intersection also further contribute to these traffic delays. The CSX railroad crossing located to the south of the intersection causes traffic delays particularly during the AM peak period. This project will address traffic delays associated with the CSX railroad crossing to the south of the US 41 and Causeway Boulevard intersection and will facilitate the safe movement of vehicle traffic through the project corridor.

In addition, this project will also address multimodal connectivity and safety within the area. Although there are sidewalks and dedicated bicycle lanes along both sides of Causeway Boulevard within the project limits, there are only sidewalks and no dedicated bicycle facilities along US 41 within the project limits. Between 2017 and 2021, there were 10 crashes involving bicyclists or pedestrians. These 10 crashes resulted in 1 fatality as well as a total of 8 injuries.

The proposed improvements have been identified in the Hillsborough County Transportation Planning Organization's (TPO) 2045 Adopted Long Range Transportation Plan (under the Hillsborough County Freight Hot Spots), the TPO's Fiscal Year 2022/23-2026/27 Transportation Improvement Program, as well as the FDOT's Statewide Transportation Improvement Plan and Strategic Intermodal System (SIS) Adopted 1st 5-Year Program. US 41 has also been identified as a Goods Movement Roadway Corridor from I-4 to the Manatee County Line and is a priority project for the National Highway Freight Program.

1.3 Existing Facility and Proposed Improvements

1.3.1 Existing Facility

The project limits identified along US 41 begin south of Denver Street (MP 22.578) and extend north of the Causeway Boulevard intersection to 23rd Avenue (MP 23.925). The improvements along Causeway Boulevard begin west of 45th Street (MP 3.554) and extend east of the Causeway Boulevard intersection terminating prior to the CSX crossing (624815B; MP 2.971). US 41 is currently

a six-lane roadway throughout the project limits and Causeway Boulevard is currently four-lanes. US 41 and Causeway Boulevard are functionally classified by the FDOT as urban principal arterials. US 41 south of Causeway Boulevard and Causeway Boulevard west of US 41 are part of FDOT's Strategic Intermodal System (SIS), designated as a SIS Connector. The CSX railroad crossing east of US 41 is a designated SIS Railway Corridor and the CSX railroad crossing south of Causeway Boulevard is designated as a SIS Railway Connector. There is one bridge culvert south of Causeway Boulevard for US 41 over Delaney Creek (MP 23.003).

US 41 from south of Denver Street to Causeway Boulevard is a divided 6-lane roadway with a 19foot median, 10-foot outside travel lanes, 11-foot middle and inside travel lanes, curb and gutter, and a sidewalk on both sides. The inside northbound travel lane from north of St. Paul Street becomes one of the two left-turn lanes for the Causeway Boulevard intersection. The sidewalk on the east side is 6-foot wide and the sidewalk on the west side varies from 5-foot to 6-foot wide.

Along US 41 from north of St. Paul Street to Causeway Boulevard, the existing typical section consists of a 5-lane curbed roadway with asphalt pavement, three travel lanes southbound and two travel lanes northbound divided by a 29-foot median. The inside northbound travel lane from north of St. Paul Street becomes one of the two left-turn lanes for the Causeway Boulevard intersection. The southbound travel lanes consist of a 10-foot outside, and 11-foot middle and inside lanes. The northbound travel lanes consist of 10-foot outside and 11-foot inside. The sidewalk on both sides varies between 5-foot to 6-foot wide.

Along US 41 from north of Causeway Boulevard to just north of S. 23rd Avenue, the existing typical section consists of an undivided 6-lane roadway with asphalt pavement, 11-foot travel lanes, a centered 10-foot bi-directional turn lane, curb and gutter, and 4-foot sidewalk along both sides of the roadway.

Along Causeway Boulevard from S. 45th Street to Sagasta Street, the existing typical section consists of an undivided 4-lane roadway with concrete pavement, 12-foot lanes, a centered 14-foot bidirectional turn lane, curb and gutter, 4-foot bike lanes, and 6-foot sidewalks.

The existing typical section of Causeway Boulevard from Sagasta Street to US 41 consists of a divided 4-lane roadway with concrete pavement and 12-foot travel lanes, 4-foot bicycle lanes, and 6-foot sidewalks on both sides.

The existing typical section of Causeway Boulevard from US 41 to the end project limits consists of a divided 4-lane roadway with concrete pavement and 12-foot travel lanes, 4-foot bicycle lanes, and 6-foot sidewalks on both sides.

The majority of the existing ROW along US 41 is 100 feet wide. In the vicinity of the CSX railroad, the ROW width varies from 100 to 332-feet. CSX Transportation owns a large portion of the adjacent property along both sides of US 41 where the CSX railroad crosses at grade. Causeway Boulevard is 150 feet wide or greater west of S. 45th Street and reduces to 100 feet wide around S. 47th Street. The ROW increases around the US 41 intersection along Causeway Boulevard then reduces to 100 feet wide before the CSX railroad crossing.

1.3.2 Proposed Improvements

This Design Change and ROW Authorization Project Development and Environment (PD&E) Reevaluation study (WPIS# 440749-1), with a 2046 Design Year, is evaluating various operational improvements along US 41/SR 45/SR 599/S. Tamiami Trail (US 41) from south of the Causeway Boulevard intersection to north of the Causeway Boulevard intersection. The study will evaluate roadway widening/reconstruction, new stormwater management facilities, new bridge overpasses at Delaney Creek, the CSX railroad, and other roadways for local traffic needs. Intersection and operational improvements being evaluated include signalization and turn lane additions for Hartford Street, US 41/Causeway Boulevard, and 47th Street. In addition to addressing operational improvements, this project will address the need for pedestrian/ bicycle accommodations and improving connectivity and safety for these modes.

There are multiple typical sections throughout the project limits. From just south of Denver Street to north of Trenton Street, the proposed typical section includes reconstructing US 41 with concrete pavement to accommodate a 6-lane divided urban curbed section with 12-foot lanes, 7-foot buffered bicycle lanes, and 10-foot sidewalks on both sides. The median width varies from 19-22 feet to provide turn lanes with raised traffic separators between opposing directions of travel. The proposed improvements will require the acquisition of ROW beyond the existing footprint varying from 0-22 feet along the west side and varying from 0-17 feet along the east side of US 41.

From north of Trenton Street the proposed typical section grade separates US 41 to continue a concrete paved typical section to south of St. Paul Street. The proposed typical section consists of a 6-lane divided urban section with concrete pavement, 12-foot lanes and 10-foot inside and outside paved shoulders. A northbound exit ramp connects to 36th Avenue with a t-intersection configuration on the east side of US 41. The proposed concrete ramp consists of a 15-foot travel lane, 7-foot buffered bicycle lane and a 10-foot sidewalk on the eastside. The existing US 41 southbound mainline pavement will be repurposed to accommodate a two-lane undivided frontage road for local access to adjacent properties. The proposed frontage road is an urban curbed section with asphalt pavement, 12-foot travel lanes, and a 10-foot sidewalk on the west side. Bridge overpasses are proposed for the US 41 mainline over Delaney Creek, 36th Avenue, and the at grade CSX Crossing (No 624802A). The proposed improvements will require the acquisition of ROW varying from 29 to 88 feet along the west side and varying from 39 to 200 feet along the east side.

From north of St. Paul Street to the Causeway Boulevard intersection, the proposed typical section along US 41 consists of a 6-lane divided urban section with concrete pavement, 12-foot lanes, 10-foot outside paved shoulders on the west side and a 7-foot buffered bicycle lane on the east side. The median bifurcates to accommodate three 12-foot left turn lanes approaching the intersection with one 12-foot right turn lane along the outside in the northbound direction. Milling and resurfacing is proposed for the outside 22-feet of the existing southbound lanes. This area will be restriped to provide a frontage road with one 15-foot lane and a 7-foot buffered bicycle lane on the outside with a new raised curb and 10-foot sidewalk. The proposed improvements will require the acquisition of ROW varying from 0 to 160 feet along the east side only.

The proposed typical section for US 41 north of Causeway Boulevard consists of a 6-lane divided urban section with 12-foot lanes, 7-foot buffered bike lanes and 6-foot sidewalks. The northbound

lanes will be asphalt and the southbound lanes will be concrete. There are two 12-foot left turn lanes and one 12-foot right turn lane shown in the southbound direction. The proposed improvements will require the acquisition of ROW varying from 30 to 45 feet along the west side and varying from 0 to 45 feet along the east side.

The proposed typical section for Causeway Boulevard from S. 45th Street to US 41 widens the existing concrete pavement to accommodate a 4-lane divided urban section with 11-foot travel lanes, 7-foot buffered bike lanes and 6-foot sidewalks along the outside. Approaching the US 41 intersection, there are two 11-foot left turn lanes and three 11-foot right turn lanes in the eastbound direction. The proposed improvements will require the acquisition of ROW varying from 0 to 44 feet along the north side only.

The proposed typical section for Causeway Boulevard from US 41 to the end project limit just west of the CSX railroad crossing consists of a westbound concrete and eastbound asphalt 4-lane divided urban section with 11-foot travel lanes, 7-foot buffered bike lanes and 6-foot sidewalks on the outside. Approaching the US 41 intersection, there are two 11-foot left turn lanes and one 11-foot right turn lane in the westbound direction. The proposed improvements will require the acquisition of ROW varying from 0 to 4 feet along the north side only.

1.4 Report Purpose

The purpose of this Noise Study Report is to document the noise analysis performed to support decisions related to the evaluation of the project Preferred Alternative and to summarize potential noise impacts to the project area. This Noise Study Report was conducted in accordance with the PD&E Manual and applicable State and Federal natural resources regulations.

2 METHODOLOGY

The traffic noise analysis was prepared in accordance with all applicable guidelines as stated within both Title 23, Part 772 of the Code of Federal Regulations (23 CFR 772) and Part 2, Chapter 18 of the FDOT's PD&E Manual (the FDOT's Noise Policy). As such, the analysis was performed using the FHWA's Traffic Noise Model (TNM, Version 2.5). Use of the TNM is required when evaluating the potential for traffic noise impacts during the design year of roadway improvement projects for which the regulations, policies, and guidelines within 23 CFR 772 and the FDOT's Noise Policy are applicable.

For properties with uses other than residential, the highway traffic noise analysis methodologies described in the FDOT's A Method to Determine Reasonableness and Feasibility of Noise Abatement at Special Use Locations were used. One special land use within the study area consists of an active sports area.

2.1 Noise Metrics

All noise levels were assessed as the hourly equivalent sound level, Leq(h), in terms of A-weighted decibels, dB(A). The hourly equivalent sound level, Leq(h), is the equivalent steady-state sound level which in a period of one hour contains the same acoustic energy as the time-varying sound level during that hour. The A-weighted decibel filtering scale applies numerical adjustments to sound frequencies to emphasize the frequencies at which human hearing is sensitive, and to minimize the frequencies to which human hearing is not as sensitive.

2.2 Traffic Data

Noise levels are low when traffic volumes are low and operating conditions are good (level of service (LOS) A or B) and when traffic is so congested that movement is slow (LOS D, E, or F). Generally, the maximum hourly noise level occurs between these two conditions (i.e., LOS C). In predicting traffic noise levels and assessing impacts, traffic characteristics that would yield the highest traffic noise level for the 2018 existing year and the 2046 design year were used. It is known that the highest traffic volume (also taking into consideration truck percentages) and the highest average speed usually create the noisiest conditions. Maximum peak-hourly traffic representing LOS C was used, unless traffic analysis shows that LOS C would not be reached. If LOS C was not reached, demand volumes were used. Detailed traffic data (e.g., motor vehicle volumes, fleet mixes, speeds) are provided in Appendix B of this NSR.

2.3 Noise Abatement Criteria

For the evaluation of traffic noise, the FHWA established Noise Abatement Criteria (NAC). As shown in **Table 2-1**, these criteria vary according to a properties' activity category (i.e., land use). For comparative purposes, typical noise levels for common indoor and outdoor activities are provided in **Table 2-2**.

Hourly Equivalent A-Weighted Sound Level (decibels (dB(A))										
Activity	Activity	Leq(h) ¹	Evaluation							
Category	FHWA	FDOT	Location	Activity Description						
A	57	56	Exterior	Lands on which serenity and quiet are of extraordinary significance and serve an important public need and where the preservation of those qualities is essential if the area is to continue to serve its intended purpose.						
B ²	67	66	Exterior	Residential						
C ²	67	66	Exterior	Active sport areas, amphitheaters, auditoriums, campgrounds, cemeteries, daycare centers, hospitals, libraries, medical facilities, parks, picnic areas, places of worship, playgrounds, public meeting rooms, public or nonprofit institutional structures, radio studios, recording studios, recreation areas, Section4(f) sites, schools, television studios, trails, and trail crossings						
D	52	51	Interior	Auditoriums, day care centers, hospitals, libraries, medical facilities, places of worship, public meeting rooms, public or nonprofit institutional structures, radio studios, recording studios, schools, and television studios						
E ²	72	71	Exterior	Hotels, motels, offices, restaurants/bars, and other developed lands, properties or activities not included in A-D or F						
F		-		Agriculture, airports, bus yards, emergency services, industrial, logging maintenance facilities, manufacturing, mining, rail yards, retail facilities, shipyards, utilities (water resources, water treatment, electrical), and warehousing						
G				Undeveloped lands that are not permitted						
 The Leq(h) activity criteria values are for impact determination only and are not design standards for noise abatement measures. Includes undeveloped lands permitted for this activity category. Note: FDOT defines that a substantial noise increase occurs when the existing noise level is predicted to be exceeded by 15 decibels or more as a result of the transportation improvement project. When this occurs, the requirement for abatement consideration will be followed 										
Sources: Tab	Sources: Table 1 of 23 CER Part 772 and Table 18 1 of Chapter 18 of the EDOT's PD&E Manual Part 2 (dated 7-1-2020)									

Table 2-1: Noise Abatement Criteria

In determining traffic noise impacts for properties with Activity Category A, B, C or E, areas of frequent exterior human use should be identified. For those properties with Activity Category D, interior areas of frequent human use should be identified. Unless the area of exterior frequent human use is identified elsewhere, residential receptor sites are be placed at the edge of the dwelling unit closest to the major traffic noise source

When more than one unit is clustered together, a single receptor can be analyzed as representative of a group of noise sensitive sites. Each residence in a multifamily dwelling is counted as one receptor when determining impacted and benefited receptors. Noise sensitive receptors may also consist of

parks, schools, hospitals, and other sites where quiet is important for normal activities. The location of the receptor in these cases will be dictated by the location of the noise source and the exterior activity that may be impacted, if any.

Common Outdoor Noise Levels	Noise Level (dB(A))	Common Indoor Noise Levels
	110	Rock Band
Jet Flyover at 1,000 feet	100	Inside Subway Train (NY)
Gas Lawn Mower at 3 feet		
Diesel Truck at 50 feet	90	Food Blender at 3 feet
Noisy Urban Daytime	80	Garbage Disposal at 3 feet
Gas Lawn Mower at 100 feet	70	Vacuum Cleaner at 10 feet
Commercial Area		Normal Speech at 3 feet
	60	
		Large Business Office
Quiet Urban Daytime	50	Dishwasher Next Room
Quiet Urban Nighttime	40	Small Theater, Large Conference Room (Background)
Quiet Suburban Nighttime		Library
	30	
Quiet Rural Nighttime		Bedroom at Night, Concert Hall (Background)
	20	
		Broadcast and Recording Studio
	10	
	0	Threshold of Hearing
Source: California Dept. of Transportation Technical Noi	se Supplement, Septembe	r 2013.

Table 2-2: Typical Noise Levels

FHWA regulations also state that a traffic noise impact is predicted to occur when predicted traffic noise levels with a proposed improvement are considered substantial when compared to existing levels. The FDOT considers a substantial increase to occur when traffic noise levels are predicted to increase 15 dB(A) or more above existing levels as a direct result of a transportation improvement project.

2.4 Noise Abatement Measures

When traffic noise impacts are predicted, noise abatement measures are considered for the impacted properties and the feasibility and reasonableness of providing an abatement measure are considered. Feasibility factors are related to the acoustical and engineering properties of an abatement measure while reasonableness factors relate to the social, economic, and environmental properties of a measure. The following subsections of this NSR present and discuss four methods of abating traffic noise impacts.

2.4.1 Traffic Management

Some types of traffic management reduce noise levels. For example, trucks can be prohibited from certain streets and roads, or be permitted to only use certain streets and roads during daylight hours. The timing of traffic lights can also be changed to smooth out the flow of traffic and eliminate the need for frequent stops and starts. Speed limits can also be reduced.

2.4.2 Alignment Modifications

Modifying the horizontal and / or vertical alignment of a roadway can also be an effective traffic noise mitigation measure. When the horizontal alignment is shifted (i.e., moved) away from a noise sensitive property or when the vertical alignment is shifted below (i.e., placing the roadway below the elevation of a noise sensitive land use) or above a noise sensitive property.

2.4.3 Buffer Zones

Providing a buffer between a roadway and noise sensitive land uses is an abatement measure that can minimize / eliminate noise impacts. To abate traffic noise at an existing noise sensitive land use, the property would be acquired to create a buffer zone. Buffer zones can also be used to eliminate the potential for new noise sensitive land uses to be impacted by traffic noise. For this purpose, and to encourage use of this abatement measure through local land use planning, noise contours have been developed and are further discussed in Section 4.0 of this NSR.

2.4.4 Noise Barriers

The most common type of noise abatement measure is construction of a noise barrier. Noise barriers have the potential to reduce traffic noise levels by blocking the sound path between the motor vehicles on the roadway (the source) and the noise sensitive land uses adjacent to the roadway.

To effectively reduce traffic noise a noise barrier must be relatively long, continuous (without intermittent openings) and sufficiently tall. For a noise barrier to be considered a potential abatement measure the barrier must meet the following conditions:

 Minimum Noise Reduction Requirements – A barrier must provide at least a 5 dB(A) reduction in traffic noise for two or more impacted noise sensitive receptors and provide at least a 7 dB(A) reduction (i.e., the FDOT's noise reduction design goal) for at least one impacted receptor. Receptors are discrete representative locations on a property that has noise sensitive land uses (see Table 2-1). Cost Effective Criteria – At a cost of \$30 per square foot, a barrier should not cost more than \$42,000 per benefited noise sensitive receptor (a benefited receptor is one that receives at least a 5 dB(A) reduction in noise from a mitigation measure). For special land uses (e.g., the outdoor eating area of a restaurant), the cost of a barrier should not be more than \$995,935 per person-hour per square foot (dollars / person-ft2). Notably, 23 CFR 772 and the FDOT's Noise Policy address the cost of abatement with respect to the number of modeled receptors. While the number of modeled receptors has been reported in this NSR, because a receptor can represent more than one property or multiple receptors can be modeled on a single property, cost calculations and considerations were made based on the number of benefited properties and not the number of benefited receptors.

3 TRAFFIC NOISE ANALYSIS

3.1 Noise Sensitive Receptors

As previously stated, receptors are discrete representative locations of a noise sensitive land use. The locations of the receptors evaluated for this study are shown on aerial maps provided in Appendix C. A total of 59 receptors representing 55 properties for which the land use has a NAC were evaluated within 13 Common Noise Environments (CNEs). A CNE is comprised of receptors within the same NAC activity category that are exposed to similar noise sources and levels. The evaluated properties represent:

- 52 residences
- 1 active sports area
- 1 restaurant
- 1 motel

Table 3-1 provides a list of the evaluated CNEs, the land use for each CNE, and the number of evaluated receptors and properties. See **Appendix C** for the Noise CNE & Monitoring Map.

CNE	Subdivision, Location or Area	Activity Category	Number of Receptors	Number of Evaluated Properties
01	Residence located on northeast corner of Sagasta Street and S 30th Avenue, south side of Causeway Boulevard	B - residential	1	1
02	Ranch House Motel (Exterior use area)	E - motel	1	1
03	Azucar Sandwich Shop (Exterior use area)	E - restaurant	1	1
04	Residences located along S 34th Avenue on the southbound side of US 41	B – residential	1	1
05	Residences located on the southbound side of US 41 (S 50th St), just south of S 34th Avenue	B - residential	2	2
06	Residences located north of Hartford Street on the northbound side of US 41	B - residential	2	2
07	Urban Core Paintball facility	C - recreation	5	1
08	Residences located south of S 24th Avenue along northbound US 41	B - residential	1	1
09	J & L Family Park mobile homes	B - residential	28	28
10	Residences located along Sagasta Street, west of US 41 (S 50th St), between S 21st Avenue and S 24th Avenue	B - residential	3	3

Table 3-1: Common Noise Environments

Residences located along El Camino			
Blanco Boulevard, north of Causeway	B - residential	6	6
Boulevard			
Residence located on eastbound El	R residential	1	1
Camino Blanco Boulevard, west of US 41	D - Tesidentiai	'	I
Residences located on the south side of S			
26th Avenue, between S 45th St and S	B - residential	7	7
47th Street			
		59	59
	Blanco Boulevard, north of Causeway Boulevard Residence located on eastbound El Camino Blanco Boulevard, west of US 41 Residences located on the south side of S 26th Avenue, between S 45th St and S 47th Street	Balanco Boulevard, north of Causeway BoulevardB - residentialBalanco BoulevardB - residentialCamino Blanco Boulevard, west of US 41B - residentialResidences located on the south side of S 26th Avenue, between S 45th St and SB - residentialAreaB - residential	Banco Boulevard, north of Causeway BoulevardB - residential6BaulevardResidence located on eastbound El Camino Blanco Boulevard, west of US 41B - residential1Residences located on the south side of S 26th Avenue, between S 45th St and SB - residential747th Street59

Most land uses were evaluated as Activity Category "B" residences. With one Activity Category "C" land use at the paintball facility, abatement would be considered if the predicted future traffic noise level with the improvements was 66 dB(A) or greater for each of these land use categories. Two Activity Category "E" land uses at the motel and sandwich shop would be considered for abatement if the future predicted traffic noise level at these locations was 71 dB(A) or greater.

3.2 Measured Sound Levels

To verify that the TNM accurately predicts existing traffic noise levels, field sound level measurements are taken. During each measurement period, average vehicle travel speeds, vehicle count and fleet identification (i.e., automobiles, trucks, buses, and motorcycles), site conditions (i.e., typography, distance from the roadway(s)) and sources of sound other than motor vehicles (e.g., aircraft flyovers, birds, barking dogs) are noted. The motor vehicle data and site conditions are used to create input for the TNM, and the model is executed. Following FDOT's methodology, the TNM is considered valid to predict existing conditions if the field measured sound levels are within 3 dB(A) of the TNM predicted highway traffic noise levels.

The field measurements were conducted in accordance with the FHWA's Measurement of Highway-Related Noise. The measurements were obtained using Rion sound level meters (SLM) Model NL-42. The SLMs were calibrated before and after each monitoring period with a Rion calibrator Model NC-74.

Short-term noise monitoring data was acquired at three (3) receptor locations within influence of highway traffic noise from Causeway Boulevard and US 41 (S 50th St) on Tuesday, April 13, 2021. Site sketch information on the noise measurements can be found in **Appendix D**. Classified vehicle traffic counts from Causeway Boulevard and US 41 (S 50th St) were acquired concurrently with each of the short-term noise monitoring sessions. Measurements were taken for three ten-minute intervals. Weather conditions for the short-term noise monitoring session were favorable for obtaining accurate noise level data.

Table 3-2 presents the field measurements and the validation results. As shown, the ability of the model to predict noise levels within the FDOT limit of plus or minus 3.0 dBA for the project was confirmed.

Receptor	CNE	Land Use NAC ¹	Date Start – Stop Time	Distance to Existing Edge of Road (feet)	TNM- Predicted L _{eq(h)} dB(A)	Measured L _{eq(h)} dB(A)	Validation Delta (Meas. – Pred.)	Validate?		
			4/13/21 11:15 – 11:24 am	45' to	70.2	73.6	3.4	Yes		
M-01	13	В	4/13/21 11:25 – 11:34 am	Causeway Blvd	70.1	73.5	3.4	Yes		
			4/13/21 11:55 – 12:04 pm		70.0	72.9	2.9	Yes		
		F	4/13/21 12:25 – 12:34 pm	59' to US 41 (S 50th St)	71.7	72.9	1.2	Yes		
M-02	05		4/13/21 12:35 – 12:44 pm		71.0	72.3	1.3	Yes		
			4/13/21 12:45 – 12:54 pm		71.0	73.3	2.3	Yes		
			4/13/21 10:15 – 10:25 am	55' to US	69.1	66.5	-2.6	Yes		
M-03	09	В	4/13/21 10:25 – 10:35 am	41 (S 50th	68.6	67.8	-0.8	Yes		
			4/13/21 10:35 – 10:45 am	Sŋ	68.5	65.8	-2.7	Yes		
^{1.} Land us the ove	 Land uses in this table are identified only for the exact noise monitoring locations. Noise monitoring locations were selected to represent the overall noise environment and for optimal TNM model validation throughout each Common Noise Environment (CNE), regardless of 									

Table 3-2: TNM Validation Table

3.3 Predicted Traffic Noise Levels

land use.

The predicted existing, future No Build Alternative, and future Preferred Build Alternative traffic noise levels for each evaluated receptor are provided in **Table 3-3** provides the range of predicted traffic noise within each CNE and the number of evaluated receptors / properties at which the Preferred Build Alternative traffic noise level is predicted to approach, meet, or exceed the NAC. None of the receptors / properties are predicted to have traffic noise levels in the future with the Preferred Build Alternative that would increase substantially (i.e., 15 dB(A) or greater) when compared to existing levels.

Peak and off-peak models were calculated for each CNE since traffic is not directionally equal in both directions using Demand volumes. Therefore, nearest traffic is represented by the peak hour volumes in one model and off-peak hour volumes in the other. Noise levels shown in **Table 3-3** represent the single loudest levels between those predicted peak and off-peak traffic conditions. Future (2046) Preferred Build Alternative traffic noise levels are predicted to approach, meet, or exceed the NAC at 11 receptors, representing 11 residences.

	Noise-	Sensitive	Receptors	Pre	dicted Traffic Noise L	evels (dB(A)) ¹	
Rec. No.	Use	NAC	Address	2018 Existing ^{2,3}	2046 No-Build ^{2,3}	2046 Build ^{2,3}	Δ^4
01-B-01	Residence	В	4901 Causeway Blvd	59.8	61.6	61.4	1.6
02-E-01	Hotel	E	2909 S 50th St	71.1	73.2	69.7	-1.4
03-E-01	Restaurant	E	3137 S 50th St	73.5	75.1	67.3	-6.2
04-B-01	Residence	В	3314 Dorothy's Dream Place	62.5	64.6	63.1	0.6
05-B-01	Residence	В	4917 S 34th Ave	61.4	63.4	61.8	0.4
05-B-02	Residence	В	4917 S 34th Ave	55.8	57.9	57.4	1.6
06-B-01	Residence	В	5010 Hartford Street	59.3	61.2	64.4	5.1
06-B-02	Residence	В	5010 Hartford Street	57.9	60.1	61.6	3.7
07-C-01	Recreational	C	3378 S 50th St	61.0	62.8	65.1	4.1
07-C-02	Recreational	C	3378 S 50th St	59.2	60.9	63.9	4.7
07-C-03	Recreational	C	3378 S 50th St	57.8	59.5	63.2	5.4
07-C-04	Recreational	C	3378 S 50th St	57.5	59.3	62.9	5.4
07-C-05	Recreational	C	3378 S 50th St	59.1	60.8	63.7	4.6
08-B-01	Residence	В	5015 24th Ave 1-10	57.1	59.0	58.5	1.4
09-B-01	Residence	В	2310 S 50th St	73.1	75.0	74.0	0.9
09-B-02	Residence	В	2310 S 50th St	68.0	69.9	69.1	1.1
09-B-03	Residence	В	2310 S 50th St	66.1	68.0	67.1	1.0
09-B-04	Residence	В	2310 S 50th St	64.7	66.6	65.6	0.9
09-B-05	Residence	В	2310 S 50th St	63.3	65.2	64.0	0.7
09-B-06	Residence	В	2310 S 50th St	62.0	63.9	62.5	0.5
09-B-07	Residence	В	2310 S 50th St	60.8	62.7	61.3	0.5
09-B-08	Residence	В	2310 S 50th St	60.0	61.9	60.4	0.4
09-B-09	Residence	В	2310 S 50th St	57.8	59.6	58.5	0.7
09-B-10	Residence	В	2310 S 50th St	58.1	60.0	58.6	0.5
09-B-11	Residence	В	2310 S 50th St	60.9	62.8	61.9	1.0

Table 3-3: Predicted Traffic Noise Levels

Noise Study Report

	Noise-	Sensitive	Receptors	Predicted Traffic Noise Levels (dB(A)) ¹			
Rec. No.	Use	NAC	Address	2018 Existing ^{2,3}	2046 No-Build ^{2,3}	2046 Build ^{2,3}	Δ^4
09-B-12	Residence	В	2310 S 50th St	52.6	54.5	54.3	1.7
09-B-13	Residence	В	2310 S 50th St	52.7	54.6	53.4	0.7
09-B-14	Residence	В	2310 S 50th St	70.9	72.8	72.4	1.5
09-B-15	Residence	В	2310 S 50th St	65.5	67.4	67.0	1.5
09-B-16	Residence	В	2310 S 50th St	63.1	65.0	64.2	1.1
09-B-17	Residence	В	2310 S 50th St	61.4	63.3	62.3	0.9
09-B-18	Residence	В	2310 S 50th St	60.2	62.0	60.7	0.5
09-B-19	Residence	В	2310 S 50th St	58.9	60.7	59.2	0.3
09-B-20	Residence	В	2310 S 50th St	57.2	59.1	57.7	0.5
09-B-21	Residence	В	2310 S 50th St	55.7	57.6	56.4	0.7
09-B-22	Residence	В	2310 S 50th St	54.4	56.4	55.3	0.9
09-B-23	Residence	В	2310 S 50th St	68.0	69.8	70.0	2.0
09-B-24	Residence	В	2310 S 50th St	61.5	63.4	63.3	1.8
09-B-25	Residence	В	2310 \$ 50th St	60.2	62.1	62.2	2.0
09-B-26	Residence	В	2310 S 50th St	65.1	67.0	67.0	1.9
09-B-27	Residence	В	2310 S 50th St	62.6	64.5	64.4	1.8
09-B-28	Residence	В	2310 S 50th St	60.7	62.6	62.6	1.9
10-B-01	Residence	В	2111 S 49th St	60.5	62.4	62.6	2.1
10-B-02	Residence	В	2303 S 49th St	60.4	62.3	61.6	1.2
10-B-03	Residence	В	4901 S 23rd Ave	64.1	65.9	65.6	1.5
11-B-01	Residence	В	2604 S 47th St	57.3	58.4	60.5	3.2
11-B-02	Residence	В	4713 El Camino Blanco Blvd	57.6	58.7	60.6	3.0
11-B-03	Residence	В	4720 El Camino Blanco Blvd	58.3	59.6	62.1	3.8
11-B-04	Residence	В	4902 El Camino Blanco Blvd	58.8	60.2	63.3	4.5
11-B-05	Residence	В	4904 El Camino Blanco Blvd	60.2	61.8	64.5	4.3
11-B-06	Residence	В	4910 El Camino Blanco Blvd	62.1	63.8	65.9	3.8

	Noise	-Sensitive	Receptors	Predicted Traffic Noise Levels (dB(A)) ¹			
Rec. No. Use		NAC	Address	2018 Existing ^{2,3}	2046 No-Build ^{2,3}	2046 Build ^{2,3}	Δ^4
12-B-01	Residence	В	4711 El Camino Blanco Blvd	63.1	64.7	68.2	5.1
13-B-01	Residence	В	4503 26th Ave	59.2	60.2	59.2	0.0
13-B-02	Residence	В	4505 S 26th Ave	59.0	60.1	59.2	0.2
13-B-03	Residence	В	4507 26th Ave	58.3	59.3	58.8	0.5
13-B-04	Residence	В	4509 S 26th Ave	57.8	58.9	58.5	0.7
13-B-05	Residence	В	4511 S 26th Ave	58.0	59.0	59.1	1.1
13-B-06	Residence	В	0 47th Blvd	58.2	59.3	60.9	2.7
13-B-07	Residence	В	2701 N 47th St	59.2	60.3	62.1	2.9

¹ The loudest of Peak vs. Off-Peak traffic predicted noise levels are shown for all design years and conditions.

² An impacted CNE may not warrant abatement analysis due to many reasons, including design/construction, safety, access, right-of-way, maintenance, drainage, and utility limitations.

³Receptors with a predicted noise level that approach or exceed the NAC are highlighted red with yellow text.

 $^{4}\Delta$ is the difference of 2046 Build Conditions to 2018 Existing Worst Case. No receptors are predicted to have an increase by 15 dB(A) or more above existing. Δ 's that are predicted to be lower in the Build Year are a result of design elements that shield the receptor from the traffic source.

Predicted 2018 existing noise levels were compared to 2046 design-year no-build and build noise levels. There are no predicted substantial noise increase impacts directly associated with this project. Of the 59 receptors modeled, eleven (11) receptors were predicted to by impacted by the project. A total of nine CNEs were found to have no noise impacts for this project and four were found to be impacted, as seen on **Table 3-4**.

CNE	NAC	Receptors ³	Total Receptors in CNE	Impacted CNE? Y/N	Warrant Abatement Analysis ¹ ? Y/N	Includes Special Land Use ² ? Y/N
01	В	01-B-01	1	N	N	N
02	E	02-E-01	1	N	N	N
03	E	03-E-01	1	N	N	N
04	В	04-B-01	1	N	N	N
05	В	05-B-01, 05-B-02	2	N	N	N
06	В	06-B-01, 06-B-02	2	N	N	N
07	С	07-C-01 thru 07-C-05	5	N	N	Y
08	В	08-B-01	1	N	N	N
09	в	09-B-01 thru 09-B-04 , 09-B-05 thru 09-B-13, 09-B-14 thru 09-B-15 , 09-B-16 thru 09-B-22, 09-B-23 , 09-B-24 thru 09-B-25, 09-B-26 , 09-B-27 thru 09-B-28	28	Y	N	N
10	В	10-B-01, 10-B-02, 10-B-03	3	Y	N	N
11	В	11-B-01 thru 11-B-05, 11-B-06	6	Y	N	N
12	В	12-B-01	1	Y	N	N
13	В	13-B-01 thru 13-B-07	7	N	N	N
		TOTAL	59	4	0	1
¹ An impac	cted CNE	may not warrant abatement analysis due to many reasons, includ	ing isolated rec	eptors, design	n/construction,	safety,

Table 3-4: Noise Level Impacts by CNE

An impacted CNE may not warrant abatement analysis due to many reasons, including isolated receptors, design/construction, safety, access, right-of-way, maintenance, drainage, and utility limitations.

² Special land uses (SLU) are analyzed during the mitigation analysis, defined as an outdoor activity area at facilities such as sports areas, churches and schools where factors such as frequency and duration are assessed to determine activity level and abatement reasonableness.

³ Impacted receptors shown in bold.

3.4 Evaluation of Abatement Measures

As previously stated, when traffic noise impacts are predicted, noise abatement measures are considered for the impacted properties. The following discusses the FDOT's evaluation of each of the measures for which an overview was provided in Section 2.4 of this NSR.

3.4.1 Traffic Management

Reducing traffic speeds and / or the traffic volume or changing the motor vehicle fleet on the proposed improvements is inconsistent with the goal of improving the ability of the roadway to handle the forecast traffic volume. Therefore, traffic management measures are not considered to be a reasonable noise abatement measure for the project.

3.4.2 Alignment Modifications

A change in the horizontal or vertical alignment of a roadway may reduce noise levels at noise sensitive receptors. The proposed improvements would be constructed to follow the existing roadway alignment. Because shifting the alignment horizontally would require substantial right- of-way acquisitions and, because noise sensitive land uses are located on both sides of the roadway, a modification to the alignment for the purpose of reducing traffic impacts is not considered to be a reasonable noise abatement measure. Additionally, suppressing the roadway's vertical alignment to create a natural berm between the highway and receivers or raising the vertical alignment is not considered to be reasonable due to the cost associated with this measure.

3.4.3 Buffer Zones

As previously stated, to abate predicted traffic noise at an existing noise sensitive land use, the property would have to be acquired. The same cost-effective limit that applies to noise barriers (i.e., \$42,000 per benefited noise sensitive receptor) would apply to the purchase price of any impacted noise sensitive property. A review of data from the Hillsborough Property Appraiser indicates that the cost to acquire the developed properties adjacent to proposed improvements would exceed the cost-effective limit. Therefore, creating a buffer zone by acquiring existing noise sensitive properties is not considered to be a reasonable noise abatement measure.

3.4.4 Noise Barriers

While four impacted CNEs are predicted to be impacted, none were found to warrant mitigation analysis as it is determined that noise abatement is not feasible for these areas. As stated in the PD&E Manual section 18.2.3.3, "once a noise abatement measure is determined to be feasible, the reasonableness of noise abatement will then be determined". Therefore, mitigation must first pass a feasibility assessment before proceeding to an analysis of reasonableness. After coordination with roadway engineering teams over potential noise barrier locations, various constructability issues were identified that rendered mitigation to be not physically feasible. Specific conditions within each CNE are discussed below.

CNE 09

This CNE, located on the northbound side of US 41 (S 50th St) north of S 24th Avenue, represents the J & L Family Park mobile homes. These residences, analyzed as NAC B, have multiple driveway access directly to US 41. Existing and 2046 future no-build and build-condition hourly equivalent sound levels were predicted at 28 noise-sensitive receptors (refer to **Table 3-3**). Future build-condition noise levels approach or exceed the applicable NAC for 8 sites; no receptors are impacted by a substantial increase.

Under FDOT policy, feasibility of a noise barrier is determined by analyzing factors related to the design and construction including safety, access, barrier height, topography, drainage, utilities, maintenance of the abatement measure, maintenance access to adjacent properties, right of way, and general access to adjacent properties.

For this CNE, a potential noise barrier was considered; however, preliminary findings determined that factors such as access, right of way, utilities, constructability, and maintenance issues would significantly impact feasibility. More specifically, FDOT maintenance requirements call for a least 5 to 7 feet of buffer behind a noise barrier; a potential barrier at CNE 09 would require right of way acquisitions; a potential barrier would completely block ingress and egress access of the residences to US 41 (S 50th St); and overhead power lines present at the location of the potential barrier would cause constructability issues. Aerial and street view images that illustrate these significant feasibility issues are shown on the following pages.

A reasonableness analysis showed that a noise barrier would meet the reasonableness criteria. An 8-foot high, 330-foot-long noise barrier would meet the noise reduction design goal and remained under the cost effectiveness goal.

A noise barrier must meet both the feasible and reasonableness criteria to be recommended for further consideration. Since this noise barrier cannot be built due to construction, utility, access, maintenance and safety concerns, there are no feasible solutions available to mitigate the noise impacts for CNE 09. Therefore, a noise barrier is not recommended for further consideration.

CNE 09 Aerial View



3-11

CNE 09 Street View 1



CNE 09 Street View 2



Noise Study Report

CNE 10

This CNE is located along Sagasta Street, west of US 41 (S 50th St), between S 21st Avenue and S 24th Avenue. This CNE represents single family residences and is evaluated as NAC B. Existing and 2046 future no-build and build-condition hourly equivalent sound levels were predicted at 3 noise-sensitive receptors (refer to **Table 3-3**). Future build-condition noise levels approach or exceed the applicable NAC for one site; no receptors are impacted by a substantial increase.

Impacted receptor 10-B-03 is an isolated impacted receptor. Abatement would not be feasible because under FDOT policy, noise abatement must provide a benefit at a minimum of two impacted receptors. Therefore, based on the noise analyses performed to date, there are no feasible solutions available to mitigate the noise impact for CNE 10.

CNE 11

This CNE is located along El Camino Blanco Boulevard, north of Causeway Boulevard. Representing 6 single family residences, it is evaluated as NAC B. Existing and 2046 future no-build and build-condition hourly equivalent sound levels were predicted at 6 noise-sensitive receptors (refer to **Table 3-3**). Future build-condition noise levels approach or exceed the applicable NAC for one site; no receptors are impacted by a substantial increase.

Impacted receptor 11-B-06 is an isolated impacted receptor. Abatement would not be feasible because under FDOT policy, noise abatement must provide a benefit at a minimum of two impacted receptors. Therefore, based on the noise analyses performed to date, there are no feasible solutions available to mitigate the noise impact for CNE 11.

CNE 12

This CNE represents a single-family residence located along eastbound El Camino Blanco Boulevard, west of US 41 (S 50th St) and is evaluated as NAC B. Existing and 2046 future no-build and build-condition hourly equivalent sound levels were predicted at one noise-sensitive receptor (refer to **Table 3-3**). Future build-condition noise levels approach or exceed the applicable NAC for one site; no receptors are impacted by a substantial increase.

Impacted receptor 12-B-01 is an isolated impacted receptor. Abatement would not be feasible because under FDOT policy, noise abatement must provide a benefit at a minimum of two impacted receptors. Therefore, based on the noise analyses performed to date, there are no feasible solutions available to mitigate the noise impact for CNE 12.

4 NOISE CONTOURS

Land uses such as residences and recreational areas are considered incompatible with highway noise levels that approach or exceed the NAC. To reduce the possibility of additional traffic noise-related impacts in the future, noise level contours were developed for the improved roadway facility. These noise contours delineate the extent of the predicted traffic noise impact area from the improved roadway's edge-of-travel lane for each of the land use Activity Categories (**Table 2-1**). **Table 4-1** provides the distance from the edge-of-travel lane at which traffic noise levels are predicted to be up to 56 dB(A)—the NAC for land uses classified as Activity Category A, up to 66 dB(A)—the NAC for land uses classified as Activity Category B and C, and up to 71 dB(A)—the NAC for land uses classified as Activity Category E.

Local officials will be provided a copy of the Final NSR to promote compatibility for the land uses adjacent to the proposed improvements.

Locations	Distance from Proposed Nearest Travel Lane to Noise Contour (Feet)		
Locations	71 dB(A) NAC E	66 dB(A) NAC B & C	56 dB(A) NAC A
US 41 Between			
Causeway Blvd and S	0	180	>400
31st Ave			
US 41 Between S 31st	0	100	>400
Ave and S 34th Ave			
US 41 Between S			
34th Ave and Trenton	0	120	>400
St			
US 41 South of	100	220	>400
Trenton St			
SR 676 East of US 41	40	120	>400
US 41 North of	40	140	>400
Causeway Blvd			
Causeway Blvd West	40	100	>400
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Table 4-1: Noi	se Contour Limits
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Figure 4-1 Noise Contours for Local Officials

US 41 Between Causeway Blvd and S 31st Ave



US 41 Between S 31st Ave and S 34th Ave



US 41 Between S 34th Ave and Trenton St








5 CONSTRUCTION NOISE AND VIBRATION

Some land uses adjacent to US 41/SR 45 are identified by the FDOT to be noise- and vibrationsensitive uses (e.g., residential use). Construction of the proposed roadway improvements is not expected to have a significant noise or vibration effect. Additionally, the application of the FDOT Standard Specifications for Road and Bridge Construction may minimize or eliminate potential issues. Should unanticipated noise or vibration issues arise during the construction process, the Project Engineer, in coordination with the District Noise Specialist and the Contractor, will investigate additional methods of controlling any impact.

6 COMMUNITY COORDINATION

Details regarding the hearing process and any traffic noise-related issues raised during the hearing or in the comment period will be documented in the final NSR.

7 CONCLUSIONS

The conclusions of this traffic noise analysis are as follows:

- Predicted noise levels will create eleven (11) NAC residential land use impacts to noisesensitive receptors in CNEs 09, 10, 11 and 12.
- The proposed project will not create any additional noise impacts due substantial noise increase over predicted existing noise levels.
- No noise barriers were found to meet the criteria for both feasibility and reasonableness.

During a project's PD&E phase, the results of a traffic noise analysis and abatement evaluation are preliminary. During the project's design phase, additional feasibility and reasonableness factors are considered for the preliminary abatement measures. These feasibility factors relate to barrier design and construction (i.e., given site-specific details, can a barrier be constructed at the evaluated location), safety, access to and from adjacent properties, right-of-way requirements, maintenance, and impacts on utilities and drainage. The viewpoint of the impacted property owners (and renters if applicable) who may, or may not, desire a noise barrier, is also a factor that is considered when making a final determination to construct noise barriers as an abatement measure.

7.1 Statement of Likelihood

The Florida Department of Transportation is committed to the construction of feasible and reasonable noise abatement measures where recommended. However, based on the noise analyses performed to date, there are no feasible and reasonable solutions available to mitigate the noise impacts at CNEs 09, 10, 11, and 12. The reasonableness of providing noise abatement in the form of a noise barrier is subject to a detailed review in Design and subsequent re-evaluations.

8 **REFERENCES**

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APPENDICES

Appendix A – Contract Plans

Appendix B – Traffic Data

Appendix C – Noise CNE & Monitoring Map

Appendix D – Noise Monitoring Field Data Sheets

Appendix E – TNM Modeling Files and PDF of the NSR

APPENDIX A

Contract Plans





Bridge Construction and applicable Interim Revisions (IRs).

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NOTES TO REVIEWER

1. THE FOLLOWING DESIGN VARIATIONS HAVE BEEN IDENTIFIED FOR THE PROJECT:

- a. BASE CLEARANCE
- b. BIKE LANE WIDTH
- c. BORDER WIDTH
- c. CURB USE HIGH SPEED
- d. SHOULDER WIDTH
- 2. PROPOSED R/W SHOWN IN THE PLANS IS PRELIMINARY AND SUBJECT TO CHANGE BASED ON THE POND SITING ANALYSIS AND FUTURE DESIGN CHANGES AS A RESULT OF THE BRIDGE DEVELOPMENT REPORT.
- 3. TRAFFIC DATA WILL BE ADDED TO THE PLAN SET WHEN IT IS MADE AVAILABLE.
- 4. THE CURB USE AND TYPE ALONG US 41 (SR 45) WILL BE DISCUSSED WITH THE DEPARTMENT DURING THE 15% LINE AND GRADE MEETING.
- 5. DURING THE PD&E PHASE, COORDINATION WITH THE HILLSBOROUGH COUNTY MPO ULTIMATELY DETERMINED THE WIDE SIDEWALK COMMITMENT TO PROVIDE 10-FOOT SIDEWALKS ALONG US 41 SOUTH OF THE CAUSEWAY BLVD. INTERSECTION.

	REVI	SIONS				STATE OF FI	ORIDA	
DATE	DESCRIPTION	DATE	DESCRIPTION	Kisinger Campo & Associates Corp.	DEP	ARTMENT OF TRAN	NSPORTATION	
				Tampa, Florida 33602	ROAD NO.	COUNTY	FINANCIAL PROJECT ID	
				Engineer of Record: Branan R. Anderson, PE P.E. No.: 78438	SR 45	HILLSBOROUGH	440749-1-52-01	
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NOTES TO REVIEWER

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US 41 Facility Parameters	Interchange	North/South of Causeway	Ramps	Sidestreets	Frontage Road	2022 FDM	2022 FDM Ramps	Design Variation
Parameter	Determination	Determination	Determination	Determination	Determination	Documentation	Documentation	Determination
1 Fuctional Classification	Urban Principal Arterial	Urban Principal Arterial	Urban Principal Arterial	Urban Principal Arterial	Urban Principal Arterial	SLD	SLD	N/A
2 Context Classification	C3C - Suburb. Comm.	C3C - Suburb. Comm.	C3C - Suburb. Comm.	C3C - Suburb. Comm.	C3C - Suburb. Comm.	EDOT Memo	EDOT Memo	
	(35 - 55 mph)	(35 - 55 mph)	(35 - 55 mph)	(35 - 55 mph)	(35 - 55 mph)	1 DOT Metho	1 DOT MEINO	N/A
3 Minimum Design Speed (SIS)	50 mph	50 mph	50 mph	N/A	N/A	Table 201.5.1	Table 201.5.2	N/A
4 Posted Speed	50 mph	50 mph	N/A	TBD	TBD	N/A	N/A	N/A
5 Proposed Design Speed	50 mph	50 mph	40 mph	35 mph	35 mph	Table 201.5.1	Table 201.5.2	N/A
			· · ·		•			
US 41 Typical Section Parameters	Interchange	North/South of Causeway	Ramps	Sidestreets	Frontage Road	2022 FDM	2022 FDM Ramps	Design Variation
Parameter	Required (Ft.)	Required (Ft.)	Required (Ft.)	Required (Ft.)	Required (Ft.)	Documentation	Documentation	Determination
1 Type of Shoulder	High Speed Curbed	High Speed Curbed	Curbed	Curbed	Curbed	Section 210.5	N/A	Yes
2 Minimum Lane Width (Travel / Auxilary)	(12 / 12)	(12 / 12)	15 (1-Lane)	(10/10)	(11/11)	Table 210.2.1	Table 211.2.1	N/A
3 Minimum Median Width (Without Barrier)	30	30	N/A	22	22	Table 210.3.1	N/A	N/A
4 Minimum Shoulder Width						Table 210.4.1		Yes
a. Outside (Full / Paved)	(10/5)	(10/5)	(10/5)	(10/5)	(10/5)	Section 210.4	Table 211.4.1	Yes
b. Inside (Full / Paved)	(10/4)	(10/4)	N/A - Curbed	N/A - Curbed	N/A - Curbed			Yes
5 Minimum Border Width	29	29	12	12	12	Table 210.7.1	Table 210.7.1	Yes
7 Minimum Sidowalk Width	(24 / 14)	(24 / 14)	(24 / 14)		(14 / 10)	Table 215.2.1	Table 215.2.1	N/A
8 Minimum Bike Lane Width	7	0 7	7	7	0 7	Section 222.1.1	Section 223 2 1 1	Ves
9 Maximum Tangent Travel Lane Cross Slopes	3.00%	3.00%	2.00%	2%	2%	Figure 210.2.1	Figure 210 2 1	N/A
10 Maximum Tangent Shoulder Cross Slopes	5.0070	5.0070	2.00/0	270	2/0	1. 1501 C 210.2/1	. 1941 C 210.2.1	
	6.00%	6.00%	Match Traval Lana	Match Traval Lana	Match Traval Jana	Section 210.4.1	Section 210.4.1	N/A
a. Outside Shoulder	5.00%	5.00%	Match Travel Lane	Match Travel Lane	Match Travel Lane		500000000000000000000000000000000000000	N/A N/A
b. Inside Shoulder	5.00%	5.00%						N/A
US 41 Horizontal Geometry	Interchange	North/South of Causeway	Ramps	Sidestreets	Frontage Road	2022 FDM	2022 FDM Ramps	Design Variation
Parameter	Required (Ft.)	Required (Ft.)	Required (Ft.)	Required (Ft.)	Required (Ft.)	Documentation	Documentation	Determination
1 Maximum Deflection (<i>Without Horiz. Curve</i>)	0°45'00''	0°45'00''	2°00'00"	2°00'00''	2°00'00"	Section 210.8.1	Section 211.7.1	N/A
2 Desired Horizontal Curve Length (400 ft Min.)	750	750	600	525	525	Table 210.8.1	Table 211.7.1	N/A
a Minimum Horizontal Curve Radius	69/	694	/132	102	402	Table 210 8 2	Table 210 8 2	N/A
	0.10	0.10	0.10	9.0E		10010 210.0.2	14510 210.0.2	
4 Maximum Super-Elevation Rate [e]	0.10	0.10	0.10	0.03	0.03	Section 210.9	Section 210.9	N/A
$rac{1}{2}$	9227 / 604	9227 / 604	E E60 / 422	NI / A	N/A	Table 210.0.1	Table 210.0.1	N/A N/A
a. $(e = NC / e max = 0.10)$ b. $(e = NC / e max = 0.05)$	8337/ 694 N/Δ	8337/ 094 N/Δ	5,560 / 452 N/A	N/A 1 1/6 / /02	1 1/6 / /02	Table 210.9.1	Table 210.9.1	N/A N/A
6 Superelevation Transition	1.160	1.160	1.175	1.100	1,1407 402	Table 210.9.2	Table 210.9.2	N/A N/A
	1.100	1.100	1.175	1.100	1.100	10510 210.5.5	10510 210.5.5	
US 41 Vertical Geometry	Interchange	North/South of Causeway	Ramps	Sidestreets	Frontage Road	2022 FDM	2022 FDM Ramps	Design Variation
Parameter	Required (Ft.)	Required (Ft.)	Required (Ft.)	Required (Ft.)	Required (Ft.)	Documentation	Documentation	Determination
1 Maximum Grade	6.00%	6.00%	6.00%	7,00%	7.00%	Table 210.10.1	Table 211.9.1	N/A
2 Minimum K-Values								N/A
a. Sag	96	96	64	49	49	Table 210.10.3	fable 211.9.2	N/A
b. Crest	136	136	70	47	47			N/A
sivinimum vertical Curve Lengths	200.4	200.64	120.4	105 ft	10F ft	Table 210 10 4	Table 211 0 2	N/A
a. sag	200 ft	200 ft	120 ft	105 TT 105 ft	105 TT	14016 210.10.4	Table 211.9.3	N/A
4 Minimum Vertical Clearance	50010	500 IL	12011	10211	10211		+	Ν/Α Ν/Δ
a. Base over BCWE (ft)	3 ft	3 ft	2 ft	2 ft	2 ft			N/A
b. Sign over Roadway (ft)	17.5 ft	17.5 ft	17.5 ft	17.5 ft	17.5 ft	Section 210.10.3	Section 210.10.3	N/A
c. Roadway over Roadway (ft)	16.5 ft	16.5 ft	16.5 ft	16.5 ft	16.5 ft			N/A
d. Roadway over Railroad (ft)	23.5 ft	23.5 ft	23.5 ft	23.5 ft	23.5 ft	1 abie 260.6.1	Table 260.6.1	N/A
5 Minimum Stopping Sight Distance								N/A
a. Downgrade (<i>ft</i>) (<u><</u> 2% / 6%)	(425' / 474')	(425' / 474')	(305' / 333')	(250' / 271')	(250' / 271')	Table 210.11.1	Table 211.10.2	N/A
b. Upgrade (<i>ft</i>) (<u><</u> 2% / 6%)	(425' / 388')	(425' / 388')	(305' / 278')	(250' / 229')	(250' / 229')			N/A
	REVISIONS						STATE OF FLO	DRIDA
DATE DESCRIPTION	DATE	DESCRIPTIO	N	Kisinger Campo & Assoc 201 N. Franklin Street, Suite Tampa, Florida 33602	ciates Corp.	DEPARTM ROAD NO.	COUNTY	SPORTATION
				Engineer of Record: Branan P.E. No.: 78438	R. Anderson, PE	SR 45 HI	LLSBOROUGH	440749-1-52-01

DESIGN CRITERIA TABLE (1 OF 2)

SHEET NO.

1B

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Causeway Blvd. Facility Parameters	Interchange	West of US 41	East of US 41	2022 FDM	Design Variation			
Parameter	Determination	Determination	Determination	Documentation	Determination			
uctional Classification	Urban Principal Arterial	Urban Principal Arterial	Urban Principal Arterial	SLD	N/A			
Context Classification	C3C - Suburb. Comm. (35 - 55 mph)	C3C - Suburb. Comm. (35 - 55 mph)	C3C - Suburb. Comm. (35 - 55 mph)	FDOT Memo	N/A			
Minimum Design Speed (SIS)	50 mph	50 mph	50 mph	Table 201 5 1	N/A			
Doctod Spood	55 mph	at mph	30 mph	Table 201.5.1	IN/A			
Posted Speed	45 mph	45 mph	45 mph	N/A	N/A			
Proposed Design Speed	45 mph	45 mph	45 mph	Table 201.5.1	N/A			
Causeway Blvd. Typical Section Parameters	Interchange	West of US 41	East of US 41	2022 FDM	Design Variation			
Parameter	Required (Ft.)	Required (Ft.)	Required (Ft.)	Documentation	Determination		•	
Type of Shoulder	Curbed	Curbed	Curbed	Section 210.5	No			
Minimum Lane Width (Travel / Auxilary)	(11/11)	(11/11)	(11/11)	Table 210.2.1	N/A			
Vinimum Median Width (Without Barrier)	22	22	22	Table 210.3.1	N/A			
Minimum Shoulder Width (3 Travel Lanes)					Ves			
a Outside (Full / Paved)	(10/5)	(10/5)	(10/5)	Table 210.4.1	Ves			
h Inside (Full / Paved)	(10/0)	(10/0)	(10/0)		Voc			
Minimum Shoulder Width /2 Travel Lanes	(10/0)	(10/0)	(10/0)		105			
a lastida (full / Save 1)	leo Int	(10/5)	(sole)	Table 210 / 1	Yes			
a. Inside (Full / Paved)	(10/5)	(10/5)	(10/5)	Table 210.4.1	Yes			
b. Inside (Paved / Full)	(8/0)	(8/0)	(8/0)		Yes			
Minimum Border Width	14	14	14	Table 210.7.1	Yes			
Minimum Clear Zone Width (Travel / Auxilary)	(24/14)	(24 / 14)	(24 / 14)	Table 215.2.1	N/A			
Minimum Sidewalk Width	6	6	6	Table 222.1.1	N/A			
Minimum Bike Lane Width	7	7	7	Section 223.2.1.1	N/A			
Maximum Tangent Travel Lane Cross Slopes	3.00%	3.00%	3.00%	Figure 210.2.1	N/A		·	
Maximum Tangent Shoulder Cross Slopes					N/A			
a. Outside Shoulder	6.00%	6.00%	6.00%	Section 210.4.1	N/A			
b. Inside Shoulder	5.00%	5.00%	5.00%		N/A			
Causeway Blvd Horizontal Geometry	Interchange	West of US 41	Fast of US 41	2022 FDM	Design			
Barameter	Poguirod (Et)	Poquired (Et)	Poquirod (Et)	Documontation	Variation			
		Required (FC)		Documentation	Determination			
Maximum Deflection (<i>Without Horiz. Curve</i>)	1.00.00	1°00'00"	1*00*00*	Section 210.8.1	N/A			
Desired Horizontal Curve Length (400 ft Min.)	675	675	675	Table 210.8.1	N/A			
Minimum Horizontal Curve Radius	559	559	559	Table 210.8.2	N/A			
Maximum Super Flourition Data [a]	0.10	0.10	0.10	Casties 210.0	21/2			
Maximum Super-Elevation Rate [e]	0.10	0.10	0.10	Section 210.9	IN/A			
Maximum curvature					N/A			
a. (e = NC / e max = 0.10)	6878 / 559	6878 / 559	68787 559	Table 210.9.1	N/A			
Superelevation Transition	1:160	1:160	1:160	Table 210.9.3	N/A			
Causeway Plud Vertical Coometry	Interchange	Wast of US 41	Frat of US A1	2022 504	Design			
Cuusewuy bivu. verticui Geometry	interchange	West 0 0341	Lust 0j 05 41	20221000	14			
,,					variation			
Darameter	Poquired (Ft.)	Popuired (Ft.)	Required (5t)	Documentation	Variation			
Parameter	Required (Ft.)	Required (Ft.)	Required (Ft.)	Documentation	Determination			
Parameter Maximum Grade	Required (Ft.) 6.00%	Required (Ft.) 6.00%	Required (Ft.) 6.00%	Documentation Table 210.10.1	Determination			
Parameter Maximum Grade Maximum Grade Change (Without Vertical Curve)	Required (Ft.) 6.00% 0.70%	Required (Ft.) 6.00% 0.70%	Required (Ft.) 6.00% 0.70%	Documentation Table 210.10.1 Table 210.10.2	Variation Determination N/A N/A			
Parameter Maximum Grade Maximum Grade Change (Without Vertical Curve) Minimum K-Values	Required (Ft.) 6.00% 0.70%	Required (Ft.) 6.00% 0.70%	Required (Ft.) 6.00% 0.70%	Documentation Table 210.10.1 Table 210.10.2	Variation Determination N/A N/A N/A			
Parameter Maximum Grade Maximum Grade Change (<i>Without Vertical Curve</i>) Minimum K-Values a. Sag	Required (Ft.) 6.00% 0.70% 96 107	Required (Ft.) 6.00% 0.70% 96	Required (Ft.) 6.00% 0.70% 96	Documentation Table 210.10.1 Table 210.10.2 Table 210.10.3	Variation Determination N/A N/A N/A N/A			
Parameter Maximum Grade Maximum Grade Change (<i>Without Vertical Curve</i>) Minimum K-Values a. Sag b. Crest	Required (Ft.) 6.00% 0.70% 96 136	Required (Ft.) 6.00% 0.70% 96 136	Required (Ft.) 6.00% 0.70% 96 136	Documentation Table 210.10.1 Table 210.10.2 Table 210.10.3	Variation Determination N/A N/A N/A N/A N/A N/A			
Parameter Maximum Grade Maximum Grade Change (<i>Without Vertical Curve</i>) Minimum K-Values a. Sag b. Crest Minimum Vertical Curve Lengths	Required (Ft.) 6.00% 0.70% 96 136	Required (Ft.) 6.00% 0.70% 96 136	Required (Ft.) 6.00% 0.70% 96 136	Documentation Table 210.10.1 Table 210.10.2 Table 210.10.3	Variation Determination N/A N/A N/A N/A N/A N/A N/A			
Parameter Maximum Grade Maximum Grade Change (<i>Without Vertical Curve</i>) Minimum K-Values a. Sag b. Crest Minimum Vertical Curve Lengths a. Sag	Required (Ft.) 6.00% 0.70% 96 136 125	Required (Ft.) 6.00% 0.70% 96 136 125	Required (Ft.) 6.00% 0.70% 96 136 125	Documentation Table 210.10.1 Table 210.10.2 Table 210.10.3 Table 210.10.4	Variation Determination N/A N/A N/A N/A N/A N/A N/A			
Parameter Maximum Grade Maximum Grade Change (<i>Without Vertical Curve</i>) Minimum K-Values a. Sag b. Crest Minimum Vertical Curve Lengths a. Sag b. Crest b. Crest	Required (Ft.) 6.00% 0.70% 96 136 125 125 125	Required (Ft.) 6.00% 0.70% 96 136 125 125	Required (Ft.) 6.00% 0.70% 96 136 125 125	Documentation Table 210.10.1 Table 210.10.2 Table 210.10.3 Table 210.10.4	Variation Determination N/A N/A N/A N/A N/A N/A N/A N/A			
Parameter Maximum Grade Maximum Grade Change (Without Vertical Curve) Vinimum K-Values a. Sag b. Crest Minimum Vertical Curve Lengths a. Sag b. Crest b. Crest Minimum Vertical Curve Lengths a. Sag b. Crest b. Crest Minimum Vertical Clearance	Required (Ft.) 6.00% 0.70% 96 136 125 125 125	Required (Ft.) 6.00% 0.70% 96 136 125 125	Required (Ft.) 6.00% 0.70% 96 136 125 125	Documentation Table 210.10.1 Table 210.10.2 Table 210.10.3 Table 210.10.4	Variation Determination N/A			
Parameter Maximum Grade Maximum Grade Change (Without Vertical Curve) Minimum K-Values a. Sag a. Sag b. Crest Winimum Vertical Curve Lengths a. Sag b. Crest Minimum Vertical Curve Lengths a. Sag b. Crest Winimum Vertical Clearance a. Base over BCWE (ft)	Required (Ft.) 6.00% 0.70% 96 136 125 125 3 ft	Required (Ft.) 6.00% 0.70% 96 136 125 125 3 ft	Required (Ft.) 6.00% 0.70% 96 136 125 125 125 3 ft	Documentation Table 210.10.1 Table 210.10.2 Table 210.10.3 Table 210.10.4	Variation Determination N/A			
Parameter Maximum Grade Maximum Grade Change (Without Vertical Curve) Minimum K-Values a. Sag b. Crest Minimum Vertical Curve Lengths a. Sag b. Crest Winimum Vertical Curve Lengths a. Sag b. Crest Minimum Vertical Clearance a. Base over BCWE (ft) b. Sign over Roadway (ft)	Required (Ft.) 6.00% 0.70% 96 136 125 125 125 125 125 125 125 125 125	Required (Ft.) 6.00% 0.70% 96 136 125 125 125 125 125 125 125 125	Required (Ft.) 6.00% 0.70% 96 136 125 125 125 125 17.5 ft	Documentation Table 210.10.1 Table 210.10.2 Table 210.10.3 Table 210.10.4 Section 210.10.3	Variation Determination N/A			
Parameter Maximum Grade Maximum Grade Change (Without Vertical Curve) Minimum K-Values a. Sag b. Crest Minimum Vertical Curve Lengths a. Sag b. Crest Winimum Vertical Clearance a. Base over BCWE (ft) b. Sign over Roadway (ft) c. Roadway over Roadway (ft)	Required (Ft.) 6.00% 0.70% 96 136 125 125 125 125 125 125 125 125 125 125 125 125 125 125	Required (Ft.) 6.00% 0.70% 96 136 125 125 125 125 125 125 125 125 125 125 125 125 125 16.5 ft	Required (Ft.) 6.00% 0.70% 96 136 125 125 3 ft 17.5 ft 16.5 ft	Documentation Table 210.10.1 Table 210.10.2 Table 210.10.3 Table 210.10.4 Section 210.10.3 Table 260.6 1	Variation Determination N/A			
Parameter Maximum Grade Maximum Grade Change (Without Vertical Curve) Winimum K-Values a. Sag b. Crest Winimum Vertical Curve Lengths a. Sag b. Crest Winimum Vertical Clearance a. Base over BCWE (ft) b. Sign over Roadway (ft) c. Roadway over Roadway (ft) d. Roadway over Railroad (ft)	Required (Ft.) 6.00% 0.70% 96 136 125 125 3 ft 17.5 ft 16.5 ft 23.5 ft	Required (Ft.) 6.00% 0.70% 96 136 125 125 125 125 125 125 125 125 125 125 125 125 125 136	Required (Ft.) 6.00% 0.70% 96 136 125 125 3 ft 17.5 ft 16.5 ft 23.5 ft	Documentation Table 210.10.1 Table 210.10.2 Table 210.10.3 Table 210.10.4 Section 210.10.3 Table 260.6.1	Variation Determination N/A			
Parameter Maximum Grade Maximum Grade Change (Without Vertical Curve) Minimum K-Values a. Sag b. Crest Minimum Vertical Curve Lengths a. Sag b. Crest Winimum Vertical Clearance a. Base over BCWE (ft) b. Sign over Roadway (ft) c. Roadway over Roadway (ft) d. Roadway over Railroad (ft) Winimum Stopping Sight Distance	Required (Ft.) 6.00% 0.70% 96 136 125 125 3 ft 17.5 ft 16.5 ft 23.5 ft	Required (Ft.) 6.00% 0.70% 96 136 125 125 3 ft 17.5 ft 16.5 ft 23.5 ft	Required (Ft.) 6.00% 0.70% 96 136 125 125 3 ft 17.5 ft 16.5 ft 23.5 ft	Documentation Table 210.10.1 Table 210.10.2 Table 210.10.3 Table 210.10.4 Section 210.10.3 Table 260.6.1	Variation Determination N/A			
Parameter Maximum Grade Maximum Grade Change (Without Vertical Curve) Minimum K-Values a. Sag b. Crest Minimum Vertical Curve Lengths a. Sag b. Crest Minimum Vertical Clearance a. Base over BCWE (ft) b. Sign over Roadway (ft) c. Roadway over Roadway (ft) d. Roadway over Railroad (ft) Minimum Stopping Sight Distance a. Downgrade (ft) (<2% / 6%)	Required (Ft.) 6.00% 0.70% 96 136 125 125 3 ft 17.5 ft 16.5 ft 23.5 ft (360 / 400)	Required (Ft.) 6.00% 0.70% 96 136 125 125 3 ft 17.5 ft 16.5 ft 23.5 ft (360 / 400)	Required (Ft.) 6.00% 0.70% 96 136 125 125 3 ft 17.5 ft 16.5 ft 23.5 ft (360 / 400)	Documentation Table 210.10.1 Table 210.10.2 Table 210.10.3 Table 210.10.4 Section 210.10.3 Table 260.6.1 Table 210.11.1	Variation Determination N/A			
Parameter Aaximum Grade Aaximum Grade Change (Without Vertical Curve) Ainimum K-Values a. Sag b. Crest Ainimum Vertical Curve Lengths a. Sag b. Crest Ainimum Vertical Clearance a. Base over BCWE (ft) b. Sign over Roadway (ft) c. Roadway over Roadway (ft) d. Roadway over Railroad (ft) Ainimum Stopping Sight Distance a. Downgrade (ft) (<2% / 6%)	Required (Ft.) 6.00% 0.70% 96 136 125 125 3 ft 17.5 ft 16.5 ft 23.5 ft (360 / 400) (360 / 331)	Required (Ft.) 6.00% 0.70% 96 136 125 125 3 ft 17.5 ft 16.5 ft 23.5 ft (360 / 400) (360 / 331)	Required (Ft.) 6.00% 0.70% 96 136 125 125 3 ft 17.5 ft 16.5 ft 23.5 ft (360 / 400) (360 / 331)	Documentation Table 210.10.1 Table 210.10.2 Table 210.10.3 Table 210.10.4 Section 210.10.3 Table 260.6.1 Table 210.11.1	Variation Determination N/A			
Parameter Maximum Grade Maximum Grade Change (Without Vertical Curve) Minimum K-Values a. Sag b. Crest Minimum Vertical Curve Lengths a. Sag b. Crest Minimum Vertical Curve Lengths a. Sag b. Crest Minimum Vertical Clearance a. Base over BCWE (ft) b. Sign over Roadway (ft) c. Roadway over Roadway (ft) d. Roadway over Railroad (ft) Minimum Stopping Sight Distance a. Downgrade (ft) (<2% / 6%)	Required (Ft.) 6.00% 0.70% 96 136 125 125 125 125 3 ft 17.5 ft 16.5 ft 23.5 ft (360 / 400) (360 / 331)	Required (Ft.) 6.00% 0.70% 96 136 125 125 125 23.5 ft (360 / 400) (360 / 331)	Required (Ft.) 6.00% 0.70% 96 136 125 125 125 125 125 125 16.5 ft 23.5 ft (360 / 400) (360 / 331)	Documentation Table 210.10.1 Table 210.10.2 Table 210.10.3 Table 210.10.4 Section 210.10.3 Table 260.6.1 Table 210.11.1	Variation Determination N/A		STATE OF F	LORIDA
Parameter Maximum Grade Maximum Grade Change (Without Vertical Curve) Minimum K-Values a. Sag a. Sag b. Crest Minimum Vertical Curve Lengths a. Sag b. Crest Minimum Vertical Clearance a. Base over BCWE (ft) b. Sign over Roadway (ft) c. Roadway over Roadway (ft) d. Roadway over Railroad (ft) Minimum Stopping Sight Distance a. Downgrade (ft) ($\leq 2\%$ / 6\%) b. Upgrade (ft) ($\leq 2\%$ / 6\%)	Required (Ft.) 6.00% 0.70% 96 136 125 125 125 125 125 125 125 125 3 ft 17.5 ft 16.5 ft 23.5 ft (360 / 400) (360 / 331) REVISIONS DATE	Required (Ft.) 6.00% 0.70% 96 136 125 125 125 125 3 ft 17.5 ft 16.5 ft 23.5 ft (360 / 400) (360 / 331)	Required (Ft.) 6.00% 0.70% 96 136 125 125 125 125 3 ft 17.5 ft 16.5 ft 23.5 ft (360 / 400) (360 / 331) Kisinger	Documentation Table 210.10.1 Table 210.10.2 Table 210.10.3 Table 210.10.4 Section 210.10.3 Table 260.6.1 Table 210.11.1	Variation N/A	DEPAR	STATE OF F RTMENT OF TRA	LORIDA NS PORTATIO.
Parameter Maximum Grade Maximum Grade Change (Without Vertical Curve) Minimum K-Values a. Sag a. Sag b. Crest Minimum Vertical Curve Lengths a. Sag b. Crest Minimum Vertical Clearance a. Base over BCWE (ft) b. Sign over Roadway (ft) c. Roadway over Roadway (ft) d. Roadway over Railroad (ft) Minimum Stopping Sight Distance a. Downgrade (ft) ($\leq 2\%$ / 6%) b. Upgrade (ft) ($\leq 2\%$ / 6%)	Required (Ft.) 6.00% 0.70% 96 136 125 125 125 125 125 125 125 3 ft 17.5 ft 16.5 ft 23.5 ft (360 / 400) (360 / 331) REVISIONS DATE	Required (Ft.) 6.00% 0.70% 96 136 125 125 125 125 3 ft 17.5 ft 16.5 ft 23.5 ft (360 / 400) (360 / 331)	Required (Ft.) 6.00% 0.70% 96 136 125 125 125 125 3 ft 17.5 ft 16.5 ft 23.5 ft (360 / 400) (360 / 331) Kisinger 201 N. Fr	Documentation Table 210.10.1 Table 210.10.2 Table 210.10.3 Table 210.10.4 Section 210.10.3 Table 260.6.1 Table 260.6.1 Table 210.11.1	Variation Determination N/A N/A <td>DEPAR</td> <td>STATE OF F. RTMENT OF TRA</td> <td>LORIDA NSPORTATIO</td>	DEPAR	STATE OF F. RTMENT OF TRA	LORIDA NSPORTATIO
Parameter Maximum Grade Maximum Grade Change (Without Vertical Curve) Minimum K-Values a. Sag b. Crest Minimum Vertical Curve Lengths a. Sag b. Crest Minimum Vertical Clearance a. Base over BCWE (ft) b. Sign over Roadway (ft) c. Roadway over Roadway (ft) d. Roadway over Roadway (ft) d. Roadway over Roadway (ft) b. Upgrade (ft) (<2% / 6%)	Required (Ft.) 6.00% 0.70% 96 136 125 125 3 ft 17.5 ft 16.5 ft 23.5 ft (360 / 400) (360 / 331) REVISIONS DATE	Required (Ft.) 6.00% 0.70% 96 136 125 125 125 3 ft 17.5 ft 16.5 ft 23.5 ft (360 / 400) (360 / 331)	Required (Ft.) 6.00% 0.70% 96 136 125 125 3 ft 17.5 ft 16.5 ft 23.5 ft (360 / 400) (360 / 400) (360 / 331) Kisinger 201 N. Fr. Tampa, F Empager	Documentation Table 210.10.1 Table 210.10.2 Table 210.10.3 Table 210.10.4 Section 210.10.3 Table 260.6.1 Table 260.6.1 Table 210.11.1	Variation Determination N/A	DEPAR ROAD NO.	STATE OF F. RTMENT OF TRA COUNTY	LORIDA NS PORTATIO FINANCIAL PR

dgrumbach



DESIGN CRITERIA TABLE (2 OF 2)

1*C*

SHEET NO.

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anorris

TYPICAL SECTION (1)

SHEET NO.

2

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anorris

- PROPOSED R/W LINE

- PROPOSED LIMITS OF CONST.

VARIES - CONC. SIDEWALK

×_×_ - NATURAL GROUND

	SHEET NO.
TYPICAL SECTION (4)	5

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anorris

¥_ — NATURAL GROUND

PROPOSED CONCRETE PAVEMENT

SHEET NO. TYPICAL SECTION (6) 7

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DESIGN SPEED = 35 MPH POSTED SPEED = 30 MPH

	REVIS	SIONS		Kisinger Campo & Associates Corp.		STATE OF F	LORIDA	
DATE	DESCRIPTION	DATE	DESCRIPTION	201 N. Franklin Street, Suite 400 Tampa, Florida 33602	DEP	ARTMENT OF TRAI	NSPORTATION	
				Engineer of Record: Branan R. Anderson, P.E.	ROAD NO.	COUNTY	FINANCIAL PROJECT ID	
				P.E. No.: 78438	SR 45	HILLSBOROUGH	440749-1-52-01	
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TYPICAL SECTION (7)

SHEET NO.

8

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	REVIS	SIONS		Kisinger Campo & Associates Corp.	1	STATE OF FI	LORIDA	í –
DATE	DESCRIPTION	DATE	DESCRIPTION	201 N. Franklin Street, Suite 400	DEP	ARTMENT OF TRAN	NSPORTATION	i i
				Tampa, Florida 33602		211(17:1514) OF 11(21)	VOI 01(1111101)	í –
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TYPICAL SECTION (8)

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TYPICAL SECTION (9)

SHEET NO.

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DATE	REVIS	SIONS DATE	DESCRIPTION	Kisinger Campo & Associates Corp.		STATE OF FL	LORIDA	
				Tampa, Florida 33602 Engineer of Record: Branan R. Anderson, P.E.	ROAD NO.	COUNTY	FINANCIAL PROJECT ID	
				P.E. No.: 78438	SR 45	HILLSBOROUGH	440749-1-52-01	
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TYPICAL SECTION (10)

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11

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APPENDIX B

Traffic Data

APPENDIX C

Noise CNE & Monitoring Map

APPENDIX D

Noise Monitoring Field Data Sheets

	RK&K	
Noise Meas	urement Data Sheet	
	1	-

Project:	VS 410 CSX	Date:	4/13/20
Meter Number	5	Traffic Monitoring Session (TMS):	TMOLGATMOR
Noise Measurement Site Number:	M-01.	Start Time:	11:15 1 11:55
File Number (on Meter):	5003 4 5005	End Time:	11:45 + 12:05 "
Location/Address:	4134 Concurry Block	Wind Speed/Direction:	El Brigh
Name of Meter Operator:	Brett Berbe		

Checklist

 Data: Fill out all data in the above table and complete this checklist.
 Announce Presence: Knock on door and leave a letter in doorway or under mat.
 Meter Location: Set meter in common use area, between building and police spurce. Minimum of 15' from building. and minimum of 50' from noise source.

Meter Height: Set microphone to 5' height.

N

<u>Meter Height</u>: Set microphone to 5 neight.
 <u>Events & Notes</u>: Record any non-traffic noise events (i.e. sirens, talking, mowers, jake brakes) or other misc, notes.
 <u>Measurements</u>: Take measurements from permanent objects on photogrammetry such as buildings or curb lines, but not trees or poles. Measure at right angles if possible and put on site sketch.
 <u>Photos</u>: Take at least 4 photos showing the entire meter including tripos. 1 towards the buildings and 1 towards the noise source, one to both remaining directions. Mark photo location on site sketch.

& vehicles twend into Alster Truck Parts

North

South

West

East

Project:	UJ41Q CSX	Date:	4/13/21
Meter Number	5	Traffic Monitoring Session (TMS):	TMOZ
Noise Measurement Site Number:	MOL	Start Time:	12:25 PM .
File Number (on Meter):	5006	End Time:	12:55 Th.
Location/Address:	3411 5 50th St	Wind Speed/Direction:	15 3.6 mil
Name of Meter Operator:	Butt Beals		
 Announce Presence: K Meter Location: Set me and minimum of 50' free Meter Height: Set micro Events & Notes: Record Measurements: Take m but not trees or poles. Photos: Take at least noise source, one to be 	Knock on door and leave a lette ater in common use area, betw m noise source. ophone to 5' height. 'd any non-traffic noise events neasurements from permanent Measure at right angles if poss 4 photos showing the entire mo oth remaining directions. Mark	er In doorway or under met. een building and noise source. M (i.e. sirens, talking, mowers, jake t objects on photogrammetry such ible and put on site sketch. eter including tripod. 1 towards th photo location on site sketch.	inimum of 15' from building brakes) or other misc. notes. I as buildings or curb lines, building and 1 towards the
Site	Sketch	Events	& Notes
P. 100 - 50 Free - 50 D 50 Town any Ar	V J HI Findeell Calbert	12:36 pm trend thele 12:38 pm Level re- 12:31 109 level may 12:47 rM level may 12:47 rM level may 12:47 rM level re- 12:51 rM decill	chittering intere horace horace it brogles it brogles it
vehicles thread	into 41 from Torrand	Frank Ave	

RK&K Noise Measurement Data Sheet
North





East







Noise Study Report

RK&K Noise Measurement Data Sheet

Project:	US41 QCSX	Date:	4/13/21
Meter Number	5	Traffic Monitoring Session (TMS):	TM03
Noise Measurement Site Number:	Mas	Start Time:	1:10 PM
File Number (on Meter):	5007	End Time:	1:40 PM
Location/Address:	2310 5 50th St	Wind Speed/Direction:	52.4 meh
Name of Meter Operator:	Britt Bank		

<u>Checklist</u> Data: Fill out all data in the above table and complete this checklist.



neighbor hood dolowing

44'

him

onh

N J

2

vehic

North





East



South

West



APPENDIX E

TNM Modeling Files and PDF of the NSR (in Project File, including "Read Me" file)



